

TN 295

.U4

IC 8787

1979









IC

8787

Bureau of Mines Information Circular/1979



## Hot-Rolling Metals in Vacuum



UNITED STATES DEPARTMENT OF THE INTERIOR



*United States Bureau of Mines.*

Information Circular, 8787

## Hot-Rolling Metals in Vacuum

By R. A. Beall, R. B. Worthington,  
and R. Blickensderfer



UNITED STATES DEPARTMENT OF THE INTERIOR  
Cecil D. Andrus, Secretary

BUREAU OF MINES  
Roger A. Markle, Director

As the Nation's principal conservation agency, the Department of the Interior has responsibility for most of our nationally owned public lands and natural resources. This includes fostering the wisest use of our land and water resources, protecting our fish and wildlife, preserving the environmental and cultural values of our national parks and historical places, and providing for the enjoyment of life through outdoor recreation. The Department assesses our energy and mineral resources and works to assure that their development is in the best interests of all our people. The Department also has a major responsibility for American Indian reservation communities and for people who live in Island Territories under U.S. administration.

TN295  
.U4  
IC 8787, 1979

This publication has been cataloged as follows:

Beall, Robert A

Hot-rolling metals in vacuum / by R. A. Beall, R. B. Worthington, and R. Blickensderfer. [Washington] : U.S. Dept. of the Interior, Bureau of Mines, 1979.

24 p. : ill. ; 27 cm. (Information circular • Bureau of Mines ; 8787)

Bibliography: p. 19-24.

1. Rolling (metal-work). 2. Vacuum metallurgy. I. Worthington, Robert B., joint author. II. Blickensderfer, Robert, joint author. III. United States. Bureau of Mines. IV. Title. V. Series: United States. Bureau of Mines. Information Circular • Bureau of Mines ; 8787.

TN23.U71 no. 8787 622.06173

U.S. Dept. of the Int. Library



## CONTENTS

|  | <u>Page</u> |
|--|-------------|
| Abstract.....  | 1           |
| Introduction.....  | 1           |
| Review of literature.....  | 2           |
| Equipment.....   | 2           |
| Properties achieved by vacuum rolling.....   | 4           |
| Bimetals.....  | 6           |
| Advantages and disadvantages of using vacuum.....  | 8           |
| Experimental procedures.....   | 9           |
| Description of equipment.....  | 9           |
| Comparison of mechanical reduction of titanium at atmospheric<br>pressure and moderate vacuum..... | 12          |
| Cladding by rolling at moderate vacuum.....  | 13          |
| Description of new equipment.....  | 16          |
| Discussion and conclusions.....  | 18          |
| References.....  | 19          |

## ILLUSTRATIONS

|  |    |
|--|----|
| 1. Vacuum rolling mill, operating side.....  | 9  |
| 2. Vacuum rolling mill, removable door.....  | 10 |
| 3. Interior of vacuum rolling mill.....  | 11 |
| 4. Effect of atmosphere on reduction of titanium.....  | 12 |
| 5. Effect of atmosphere on reduction of Ti-5Al-2.5Sn.....  | 12 |
| 6. Effect of atmosphere on reduction of Ti-6Al-4V.....   | 13 |
| 7. Interface between roll-bonded molybdenum and low-carbon steel.....  | 13 |
| 8. Interface between roll-bonded molybdenum and electrolytic iron.....   | 14 |
| 9. Thin sheets of molybdenum roll-bonded to iron.....  | 15 |
| 10. Roll-bonded sandwich of top 304 stainless steel, electrolytic iron,<br>molybdenum, and bottom 316 stainless steel..... | 16 |
| 11. Electrolytic iron-chromium bond.....   | 17 |
| 12. New facility, vacuum rolling mill.....   | 17 |

## TABLES

|   |    |
|---|----|
| 1. Roll-bond diffusion between molybdenum and electrolytic iron at<br>1 micrometer depth..... | 14 |
| 2. Roll-bond diffusion between molybdenum and steel at 1 micrometer<br>depth.....             | 14 |



# HOT-ROLLING METALS IN VACUUM

by

R. A. Beall,<sup>1</sup> R. B. Worthington,<sup>2</sup> and R. Blickensderfer<sup>2</sup>

---

## ABSTRACT

As part of an ongoing program to develop high-quality materials with improved performance and service lives, and to conserve critical minerals, Bureau of Mines, U.S. Department of the Interior, researchers studied the process of hot-rolling metals, alloys, and composites in vacuum. First, a comprehensive review of the literature is presented, including the advantages and disadvantages of using vacuum. Next, details of hot-rolling titanium, chromium, and molybdenum-iron bimetal are given. Finally, the design of new equipment is described. At this time, it is uncertain whether hot-rolling metals in vacuum will gain commercial acceptance in the future.

## INTRODUCTION

Among the significant technological accomplishments of the third quarter of the 20th century was the wide application of vacuum-to-metal melting. Many of the more common metals, as well as superior alloys of steel, have benefited from vacuum degassing, and the production of reactive and refractory metals leans heavily on vacuum-melting techniques. Fabrication and other forming operations of vacuum-melted material, carried out in air, were believed to be detrimental to the physical and mechanical properties of the finished material because of interstitial elements acquired during the forming operations.

In-Fab (55),<sup>3 4</sup> a large inert atmosphere room containing forging and rolling equipment, was built in the early 1960's through Government-industry cooperation to alleviate the problems of air fabrication. The technique was never found to be acceptable commercially in the United States. Limited studies of fabrication in a vacuum were conducted in the fabrication of refractory and

---

<sup>1</sup>Supervisory physical research scientist.

<sup>2</sup>Metallurgist.

All authors are with the Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.

<sup>3</sup>Reference to specific equipment or manufacturers is made for identification only and does not imply endorsement by the Bureau of Mines.

<sup>4</sup>Underlined numbers in parentheses refer to items in the list of references at the end of this report.

nuclear metals. A common problem in these studies was the unexpected bonding of metal when ultraclean surfaces were present in the vacuum.

The Bureau of Mines, U.S. Department of the Interior, conducted an investigation to determine whether the solution to this problem could be applied to obtain bonds between scarce and critical metals and a noncritical substrate. This method could then be used to produce thin-clad hardware, conserving chromium, nickel, and cobalt, and help achieve the Bureau's goals to minimize the requirements for scarce or critical minerals through conservation and substitution.

This report presents a review of the literature on vacuum rolling, a description of the equipment developed, experimental data obtained to date, and a brief discussion of the potential of vacuum rolling for eventual commercial adoption.

## REVIEW OF LITERATURE

### Equipment

Worldwide reviews of the vacuum-rolling equipment are given by Krupin and Yudina (39) and by Krupin (33). Beginning with the first vacuum hot rolling mill in 1953, a number of mills of increasing size and capability were developed in the U.S.S.R. The U.S.S.R. mills can be evacuated to about  $1 \times 10^{-5}$  torr and can roll at a maximum temperature of  $900^{\circ}$  to  $1,600^{\circ}$  C. The first two vacuum-rolling units, built by the Technical Institute of the Academy of Sciences of the U.S.S.R., were described by Amonenko (5) in 1960. The first consisted of a small rolling mill with work rolls 85 mm in diameter and 150 mm long. The entire mill and frame, except for the drive motor and drive gears, were located within the vacuum chamber. From experience gained with this unit, a second vacuum rolling mill was designed and constructed. This second design incorporated the "roll-chamber" concept that became standard with U.S.S.R. vacuum-rolling technology. In this design, by constructing the chamber as an integral part of the mill housing, only the rolls were enclosed in the vacuum chamber. The volume and pumping capacity required were thus minimized. The screwdowns, roll bearings, gears, etc., were outside the chamber. The first mill of this type utilized rolls 200 mm in diameter and 300 mm long with a removable barrel to facilitate roll changing. Additional vacuum chambers, attached to each side of the mill chamber, enclosed manipulators and molybdenum-wound resistance furnaces capable of  $1,500^{\circ}$  to  $1,600^{\circ}$  C. This mill was later improved, as described by Smirnov (50), and installed at the Ukrainian Scientific Institute of Metals. Krupin and Pavlov (35) described another "roll-chamber" vacuum rolling mill at the Moscow Institute of Steels and Alloys capable of operating at  $5 \times 10^{-5}$  torr. The rolls were 210 mm in diameter and 340 mm long. Krupin (33) also mentioned a two-high mill with 210-mm-diameter rolls that was enclosed in a vacuum chamber at the Leningrad Molding Institute of Kolinin before 1964. This mill was later converted to a "roll-chamber" type capable of  $1 \times 10^{-4}$  torr. Problems with manipulators including overheating when operating through the furnace were mentioned.



The Technical Institute of the Academy of Sciences of the U.S.S.R. built another two-high vacuum rolling mill of the "roll-chamber" type, reported by Sigalov and Exerskii (49) in 1968. This two-high mill utilized 400-mm-diameter by 450-mm-long rolls, a 150-kw drive motor, and was capable of  $10^{-6}$  torr. In 1961, the Physicotechnical Institute built a vacuum rolling pilot plant with six-roll stands to produce sheet and rods from chemically active metals at  $1 \times 10^{-6}$  torr, mentioned by Ivanov (27). At the All-Union Research Institute, Tsygankov and Perfil'ev (57) reported in 1961 on a fully automatic vacuum rolling plant for tube production. In 1977, Kolikov (31) found that during helical rolling of refractory metals the billet could be reduced farther before fracture of the axial zone when rolling in vacuum than when rolling in air.

Another vacuum-rolling train, utilizing 210-mm-diameter rolls and a vacuum of  $5 \times 10^{-6}$  torr, was set up at the Moscow Institute of Steel and Alloys by Krupin (37) in 1965. This mill was a two-high reversing mill with its frame located within the vacuum chamber. A vacuum furnace was located on each side of the mill. According to Krupin (33), a similar unit was operated by Smirnov (50) at the Leningrad Polytechnic Institute. Production vacuum rolling was described by Polukhin (44-45) in which steel and refractory metal tubes were helically cross-rolled. In addition, vacuum-forging equipment was described by Pevzner (43) in 1967; and an assembly for rolling pipes in inert gas, in which workers wore pneumatic clothes, is referred to by Krupin (33).

The efforts in the United States toward preventing the oxidation of metals during hot working were directed primarily toward the use of inert gas. The state-of-the-art as of 1956 for fabricating under inert gas is given in Steel (55). Kolbe (30), at the General Electric Co., forged molybdenum and tungsten at  $2,000^{\circ}$  C in inert gas. Semchyshen and Barr (48), at Climax Molybdenum Co., constructed two different argon-filled enclosures around a press and furnace. The first unit accommodated an operator wearing breathing apparatus, and the second used glove ports allowing the operator to be outside. Neither arrangement maintained sufficient purity of the argon to allow true hot working of the molybdenum ingots.

The most elaborate inert processing facility was the In-Fab room of Universal Cyclops Steel Corp. described in Steel in 1956 (55), Industrial Heating in 1962 (24), and Iron Age in 1958 (25). The 40- by 80- by 25-foot-high facility, constructed in the late 1950's, included a forging hammer, reversible rolling mill, induction furnace, and graphite furnace capable of  $2,200^{\circ}$  C as well as a lathe, saw, welder, and hot shears. The workmen were dressed in "space suits" with intake and exhaust lines. Several smaller inert gas chambers were operated by the U.S. Atomic Energy Commission as described by Kelman (28) in 1956. The operations were performed either by remote control or by workers being outside the chamber and operating with glove ports. Also, three rolling mills for radioactive metals were assembled at the University of California for operation under vacuum or inert gas described in Iron Age in 1962 (26).



Rossin and Mueller (46) reported on a small rolling mill, 3 by 5 inches, enclosed with a vacuum chamber at Universal Cyclops Steel Corp. An induction furnace, also in the chamber, permitted heating samples to  $1,650^{\circ}\text{C}$ . In 1962, Universal Cyclops proposed a large scale "Vac-Fab" rolling plant described in Steel (56), but this was never constructed. Hill (23) reported on a vacuum rolling mill at Republic Steel Corp. that was used to consolidate titanium powder to eliminate the arc-melting step. The system operated at a pressure of  $10^{-3}$  torr.

Habermann (22) described an apparatus for forging at temperatures to  $1,800^{\circ}\text{C}$  under argon. Blickensderfer (8) described laboratory equipment for heating and forging under a vacuum better than  $1 \times 10^{-4}$  torr at  $1,800^{\circ}\text{C}$ .

### Properties Achieved by Vacuum Rolling

Throughout the variety of techniques and equipment described, the literature has shown that metals rolled under vacuum usually have properties different from those rolled in air. The vacuum-rolled metals, in addition to having a superior surface finish, usually have greater ductility, improved impact strength, lower ductile-brittle-transition temperature, better corrosion resistance, and greater electrical conductivity. The rolling process itself in vacuum, contrasted with that in air, is typified by a tendency for the metal to adhere to the rolls, greater forward slip of the metal, and requires more energy.

Early investigations of vacuum rolling established that oxidation could be essentially prevented and that metals which cracked during air rolling could be successfully rolled in vacuum. Ivanov (27) hot-rolled Mo, Mo alloys, Ti, Zr, Zr alloys, Cb, and Ta under a vacuum of  $1 \times 10^{-5}$  torr. Carter (12) reported that tantalum alloys, Ta-10W and F-48, could be rolled at pressures of  $10^{-3}$  to  $10^{-4}$  torr, and that the columbium alloy D-31 and the molybdenum alloy TZM could be rolled at pressure up to  $10^{-1}$  torr. Krupin (38) rolled tungsten and molybdenum successfully in vacuum. They found that  $5 \times 10^{-3}$  torr was sufficient because no additional benefit was observed when the vacuum was increased to  $5 \times 10^{-5}$  torr. Krupin and Pavlov (36) reported an increase in ductility and oxidation resistance after vacuum rolling of W, Mo, Rh, Cb, Ta, Zr, V, Cu, Ni, and other alloys compared with rolling in air. Smirnov (54) discovered that beryllium could be rolled successfully at high speed (0.76 m/s) under vacuum of  $5 \times 10^{-5}$  torr, but it cracked when the rolling rates were low (0.1 m/s).

The early interest with vacuum rolling probably can be attributed to improved ductility. The increased ductility of metals rolled under vacuum has been reported by many investigators. It is usually, but not always, accompanied by a decrease in ultimate tensile strength. An increase in impact strength and a reduction in the ductile-brittle-transition temperature normally occur also. The greater ductility of vacuum-rolled materials is attributed to the absence of impurities, uniformity of structure, and elimination of microdefects as summarized by Krupin (33).

Smirnov (51) rolled Ti, Mo, and Cb at  $1 \times 10^{-3}$  to  $2 \times 10^{-5}$  torr and in air. The ductility was 50 to 85 percent greater and the tensile strength was 5 to 15 percent less for the specimens rolled in vacuum. Gurevich (18) compared the effect of rolling Ti, Mo, Cb, and Cr in vacuum, argon, and air. Based on oxygen and nitrogen analyses, they advised that Ti, Cb, and Cr be hot-rolled under high vacuum of about  $10^{-5}$  torr, but molybdenum could be rolled at about  $10^{-2}$  torr. In agreement with Smirnov and others, it has been reported that titanium and molybdenum have greater ductility and lower strength when rolled in vacuum than in air. Gurevich and Orzhekhovskiy (19) confirmed the preceding and reported a decrease in the ductile-brittle-transition temperature for Cb, Mo, and W rolled under vacuum. Both papers reported that rolling in inert atmosphere produced intermediate effects.

Bykadorov (10-11) reported that steels hot-rolled in vacuum exhibited approximately 2 to 60 percent decrease in yield point and ultimate tensile strength, and that the latter was more uniform. The lack of oxide eliminated the need for pickling and the lower yield point obviated the need for annealing before drawing.

Nel'zin and Filippov (40) studied titanium alloys and found that hot rolling under vacuum of  $1 \times 10^{-4}$  to  $1 \times 10^{-5}$  torr produced material without scale and with increased plasticity. The mechanical strength dropped by 7 to 10 percent while impact strength increased 10 percent. Krupin (33) reported that the ductility of cast chromium rolled in vacuum of  $5 \times 10^{-5}$  torr was increased threefold. For rhenium, the red-brittleness was avoided at a vacuum of  $10^{-1}$  to  $10^{-2}$  torr. The elongation of columbium rolled in vacuum of  $5 \times 10^{-5}$  torr was 18 percent contrasted with only 3 percent when rolled in air. The ductile-brittle-transition temperatures of chromium and tungsten were decreased  $100^{\circ}$  to  $200^{\circ}$  C by vacuum rolling. An iron alloy, N-42, had a 64 percent increase in ductility with only a slight decrease in tensile strength. Krupin and Chernyshev (34) summarized the effects of vacuum on the rolling of metals.

Many other effects of vacuum rolling have been reported in the literature. Gurevich and Zubko (21) reported that the carbon content of the surface of vacuum-rolled steel was higher than the same steel rolled in air, which normally has a depletion of surface carbon. The sulfur decreased less by rolling in vacuum than in air. Also, the coefficient of friction of the steel and its resistance to rolling deformation were greater during vacuum rolling, while specific pressure was several times larger in vacuum. Osipov (41) studied specific pressure, coefficient of friction, and forward slip during hot rolling of tungsten in vacuum. Pavlov (42) measured a coefficient of friction of 0.34 to 0.36 during vacuum rolling. Chernyshev (13) showed that the proportion of forward slip of the metal increased for titanium and molybdenum but decreased for steel when rolled in vacuum.

Krupin and Pavlov (36) reported a significant increase in the corrosion resistance to an aggressive medium of a titanium alloy, bronze, and stainless steel rolled in vacuum. An increase in oxidation resistance also was reported. For example, the oxidation rate at  $1,200^{\circ}$  C of vacuum-rolled columbium decreased to half, and that of vanadium decreased to one-third. Krupin (33) reported similar benefits to tantalum. He also reported a significant



improvement in the electrical conductivity of Zr, Cb, Ta, V, and Cu after rolling in a vacuum of  $10^{-4}$  to  $5 \times 10^{-5}$  torr.

Smirnov (53) showed that titanium, after vacuum rolling below  $10^{-4}$  torr, had a more uniform grain structure with larger grain size. Also, the fine-grain surface structure normally associated with molybdenum, and attributed to gas contamination, was eliminated by vacuum rolling. The effect of surface contamination on the microstructure of molybdenum and its alloy, TZM, is discussed in Industrial Heating (24).

Both thermodynamics and kinetics of metal-gas reactions are relevant to vacuum hot-rolling processes. Considering oxide dissociation reactions and the kinetics of oxidation, Krupin and Pavlov (36) established conditions for an oxidation-free treatment at high temperature. Metals such as W, Mo, Re, Ni, Cu, Os, and others, with relatively high dissociation pressures of the oxide, are nonoxidizing at  $10^{-1}$  to  $10^{-2}$  torr at their respective hot deformation temperatures. Theoretically, Ti, Zr, Cb, Ta, V, and other metals having oxides with extremely low vapor pressure should oxidize at pressure too low for commercial application of vacuum rolling. But in practice, because of the low rate of oxidation at low pressure,  $10^{-5}$  torr is generally sufficient to control oxidation during normal process times. A more complete discussion of basic thermodynamics and kinetics in vacuum metallurgy was presented by King (29). A mass spectrometric analysis of the gases normally encountered in vacuum rolling was made by Anikeev (6). Bianchi and Mueller (7) found that argon provided more protection to metals during hot working, for a given oxygen pressure, than did vacuum.

The problem of adherence of metals to the rolls during vacuum rolling has been reported by several investigations in the U.S.S.R. Krupin (38) reported a tendency for tungsten to adhere to the rolls at a temperature of  $1,300^{\circ}\text{C}$ . Osipov (41) experienced difficulties caused by welding of tungsten to the rolls until the rolls were coated with a hard fusible material, which was not identified. Krupin and Pavlov (36) also mentioned the adherence problem with tungsten above  $1,450^{\circ}\text{C}$ . Chernyshev (13) discussed the adherence problem and pointed out that the lack of an oxide film on the metal allowed the bond. Gurevich (20) studied diffusion of rolled metal into the rolls during hot rolling. Chernyshev (14) compared the forward slip during rolling in vacuum with that in air. Pavlov (42) reported on the effects of roll material and surface finish. Polukhin (45) reported that a boron carbide coating on the rolls prevented adhesion.

### Bimetals

Because vacuum can prevent the formation of metal oxide and nitride films during heating and rolling, there is a greater potential for the bonding of bimetal surfaces during vacuum rolling than during air rolling. Dolzhenkov and Krivonosov (15) clad titanium to steels of various carbon content by vacuum rolling. They reported that a temperature of  $1,000^{\circ}$  to  $1,050^{\circ}\text{C}$  was required to produce the best bond, but a problem with embrittlement of the interface resulted from the formation of titanium carbide. Krupin and Yudina (39) reported on results obtained by rolling composites under vacuum of

$1.5 \times 10^{-5}$  to  $5 \times 10^{-5}$  torr. Their composites consisted of commercial titanium bonded to low- and high-carbon steel, stainless steel, and manganese steel. The titanium steel bond was produced in vacuum with 20 to 30 percent reduction whereas in air a reduction of 70 to 80 percent was required. Dolzhenkov (16) studied the effects of vacuum in the range of  $10^{-2}$  to  $10^{-5}$  torr on the roll bonding of iron-titanium at  $1,000^{\circ}$  C. They obtained a shear strength of 16 to 22 kg/mm<sup>2</sup> for specimens rolled at  $10^{-4}$  to  $10^{-5}$  torr, and 3 to 16 kg/mm<sup>2</sup> for specimens rolled at  $10^{-2}$  to  $10^{-3}$  torr. Smirnov (52) bonded large sheets of titanium to steel by enclosing them in a pack which was evacuated during rolling. A shear strength of 15 to 20 kg/mm<sup>2</sup> was obtained. Amonenko (2) reported on the use of columbium and copper intermediate layers in titanium steel bonds to improve the ductility. Dolzhenkov (17) reported on the vacuum rolling of titanium steel on a pilot scale at a pressure of  $5 \times 10^{-5}$  torr. The problem of the brittle interface was overcome by using thin layers of nickel-copper at the interface. The resulting shear strength was 30 to 35 kg/mm<sup>2</sup>.

Aleksandrov (1) produced copper-nickel bimetals with bond strengths up to 25 kg/mm<sup>2</sup> by rolling in vacuum of  $10^{-4}$  torr. Rolling in a poorer vacuum of  $1 \times 10^{-1}$  torr produced bonds with 21 kg/mm<sup>2</sup> strength whereas rolling in air at  $400^{\circ}$  to  $800^{\circ}$  C produced no bonding.

Krivososov (32) determined the optimum conditions for bonding of iron and columbium at  $1,100^{\circ}$  C at  $4 \times 10^{-5}$  torr. A 10-percent rolling reduction resulted in a shear strength less than 10 kg/mm<sup>2</sup>, but with 30 to 40 percent rolling reduction the shear strength was increased to 30 to 40 kg/mm<sup>2</sup>. Amonenko (4) reported on the effect of temperature and degree of vacuum on the bonding of steels to copper, titanium, and stainless steel, as well as Cu, Ni, Cb, and Mo bonds to each other. A residual pressure greater than  $10^{-1}$  to  $10^{-2}$  torr caused low bond strength, even for copper-nickel. Amonenko (3) studied the cladding of high-purity copper-nickel for the electronics industry.

Sadaj (47) reported on rolling steel with Ti, Mo, Al, Cb, Cu, steel, Monel, NiMo alloy, and TZM. Several rolling conditions and temperatures were studied. Subsequent heat treating to promote diffusion was found detrimental to iron-molybdenum bonds because of the formation of  $\text{Fe}_7\text{Mo}_8$  or  $\text{Fe}_2\text{Mo}_2\text{C}$  intermetallic compounds.

In the United States, Bonchak and Bianchi (9) patented the method of cladding metals by rolling in argon. Columbium-molybdenum and tantalum-tungsten were successfully bonded. Winter (58) in another U.S. patent showed how to roll bond certain materials, such as copper-copper 25 percent nickel and aluminum-stainless steel, in air. His claims required that one component have a recrystallization temperature under  $260^{\circ}$  C and that the other must be at least  $60^{\circ}$  C higher.

### Advantages and Disadvantages of Using Vacuum

The advantages cited in the literature for rolling under vacuum, especially compared with rolling in air, can be summarized as follows:

1. Much less edge cracking and breaking of metal.
2. Improved surface finish.
3. Elimination of material loss caused by oxidation.
4. Improved ductility.
5. More uniform yield strength and ultimate strength among samples.
6. Improved impact strength.
7. Lower ductile-brittle-transition temperature.
8. Improved corrosion resistance.
9. Improved oxidation resistance.
10. Improved electrical conductivity.
11. Elimination of pickling step after rolling.
12. More uniform grain size.
13. Higher coefficient of friction.
14. Greater bonding strength of bimetals.
15. Positive roll bonding of bimetals not otherwise possible.
16. Less rolling reduction required to achieve a bimetal bond.

The disadvantages of vacuum rolling compared with air rolling are:

1. Inherent complications and expenses of the vacuum system.
2. Inaccessibility to the interior of the chamber.
3. Time required for pumpdown.
4. Increased rolling power required.
5. Increased roll forces (specific pressure) during rolling.
6. Tendency for some metals to adhere to the rolls at high temperature.

Although rolling metal in an inert gas system might seem at first to be more practical than rolling in a vacuum system, it is apparent, on review of the literature, that the results have not proved to be as satisfactory.



It is concluded that this is the result of the extreme difficulty in maintaining the required degree of purity in an inert gas to prevent oxidation of reactive metals. For example, only 10 ppm impurity in an inert gas gives a partial pressure of the impurity of  $7.6 \times 10^{-3}$  torr. In comparison it is not all that difficult or expensive to obtain through use of vacuum pumps a lower partial pressure of impurity gases.

## EXPERIMENTAL PROCEDURES

### Description of Equipment

Beginning in 1970, Bureau researchers assembled a vacuum rolling mill from available components, and tested some of the concepts reported in the literature. For this purpose a large cubical chamber equipped with many view-ports and manholes was available. Evacuation was provided by a mechanical pump of 250 cu ft/min ( $7 \text{ m}^3/\text{min}$ ) displacement. Ultimate vacuum of the system was  $3 \times 10^{-2}$  torr. The chamber, shown in figure 1, housed a 2- by 4-inch laboratory rolling mill. Access to the interior, which measures 60 by 70 by 66 inches

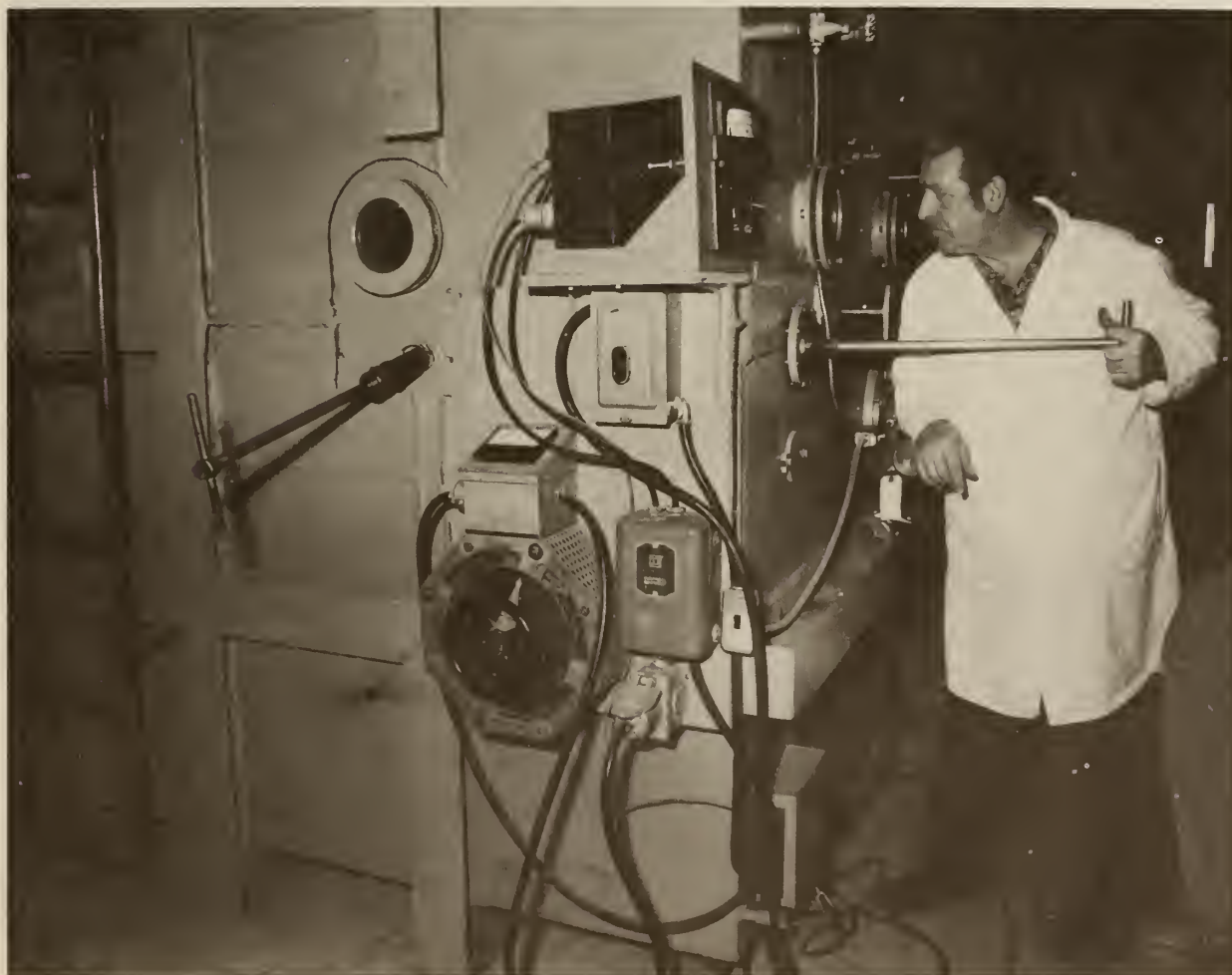


FIGURE 1. - Vacuum rolling mill, operating side.

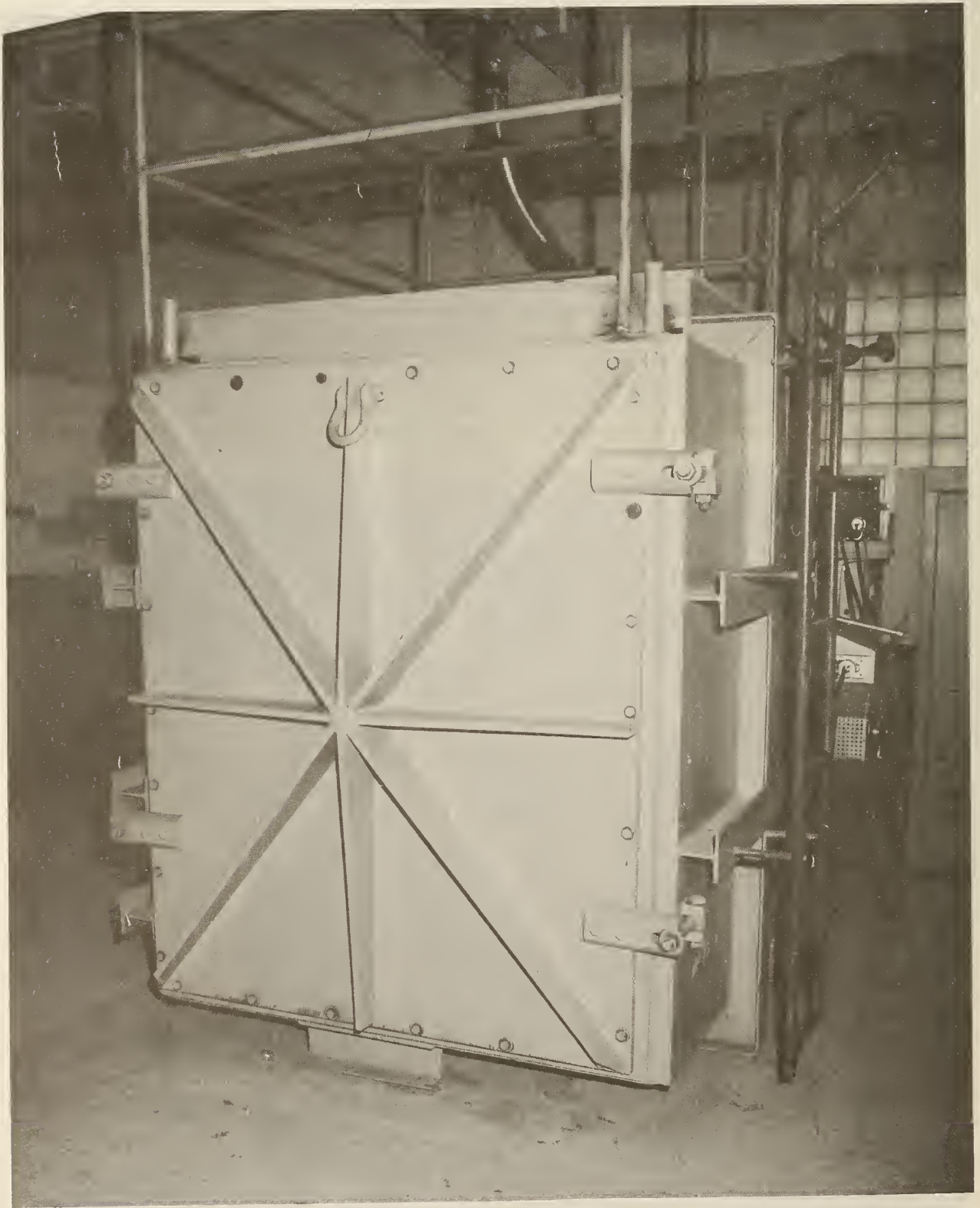


FIGURE 2. - Vacuum rolling mill, removable door.

high could readily be made through an 18-inch-diameter manhole located on top of the large chamber. When necessary, the complete rear door shown in figure 2 could be removed. The laboratory rolling mill and specimen furnace are shown in figure 3; also shown in this figure are the two manipulator arms that were used to transfer the samples from the furnace to the rolls.

A direct current (dc) motor, located inside the vacuum chamber, was used to drive the rolls to eliminate the requirement for rotating seals in the chamber wall. The low potential (48 volt) used on the motor prevented electrical arcing that would result at normal alternating current (ac) line potential under low pressure. The dc motor also was advantageous in possessing high torque at low speed. A large storage battery outside the chamber provided the power.

The samples were heated in an insulated ceramic hearth furnace with molybdenum disilicide heating elements. Although this furnace was satisfactory for this system, outgassing became a problem in a lower pressure system.



FIGURE 3. - Interior of vacuum rolling mill, viewed from top of manhole. A, Specimen furnace; B, guideway; C, roll housing; D, manipulator for sample handling.



Comparison of Mechanical Reduction of Titanium  
at Atmospheric Pressure and Moderate Vacuum

One objective of this project was to determine the effect vacuum rolling had on the mechanical properties of metals. Titanium and two titanium alloys were selected, and were rolled at three pressure levels and three temperatures. The temperatures chosen were 850°, 950°, and 1,050° C for the alloys titanium-6 aluminum-4 vanadium and titanium-5 aluminum-2.5 tin, an alpha, beta, and alpha-beta alloy. Titanium was rolled at 750°, 850°, and 1,000° C. The temperature drop between the furnace and the rolls may have been as much as 100° to 200° C. This problem was kept to a minimum by reducing the transfer time to 10 to 20 seconds; if over 30 seconds, the pass was aborted. The atmosphere of the chamber was controlled at pressure levels of  $10^{-1}$ , 1, and 760 torr.

Fifty-four samples were rolled through eight passes under the conditions stated. The percentage reduction is plotted in figures 4-6. All passes were

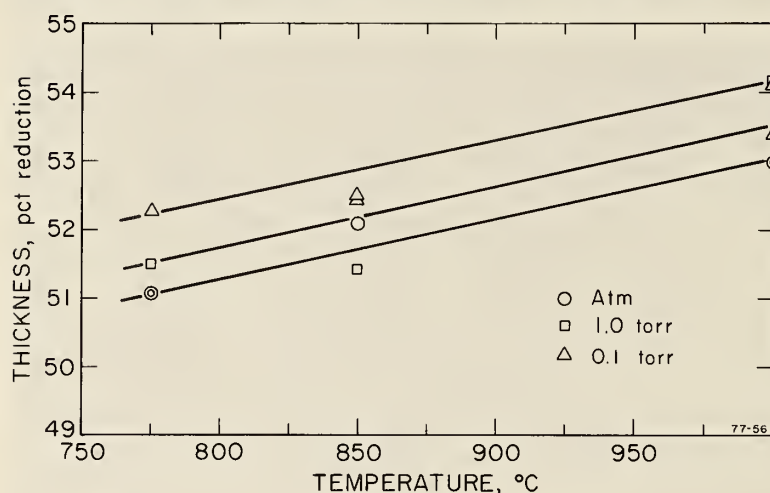


FIGURE 4. - Effect of atmosphere on reduction of titanium.

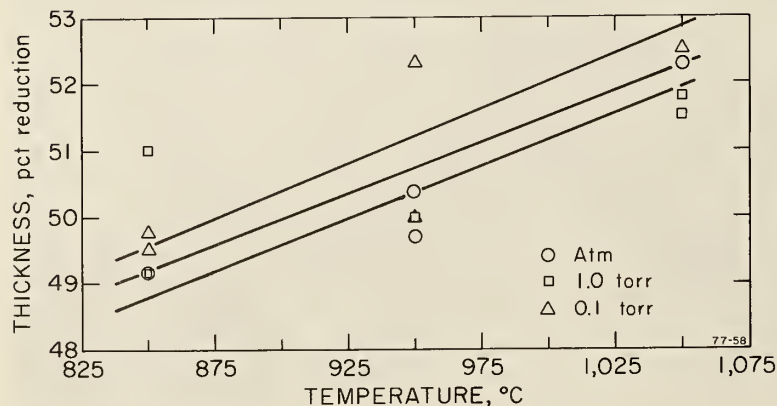


FIGURE 5. - Effect of atmosphere on reduction of Ti-5Al-2.5Sn.

made with the roll separation reduced 10 percent from the previous setting. As expected, there was a consistent change of reduction with temperature. There also was a small but noticeable increase in reduction at lower pressures. Since the temperature dependence is of greater magnitude than the pressure effect, a variation in heat loss due to inconsistent transfer time or due to change in convection could be involved.

The 54 rolled bars were straightened and machined to dimensions of a standard tensile test specimen of about 0.045 in<sup>2</sup> cross sections for tensile strength, yield strength, percent elongation, and reduction in area determinations. The results were nonconclusive. The tensile properties of these materials were not affected by air pressure in the range of  $10^{-1}$  torr to atmospheric. It is expected that much lower pressures, on the order of  $10^{-4}$  to  $10^{-6}$  torr, are needed to obtain measurable changes in these properties.

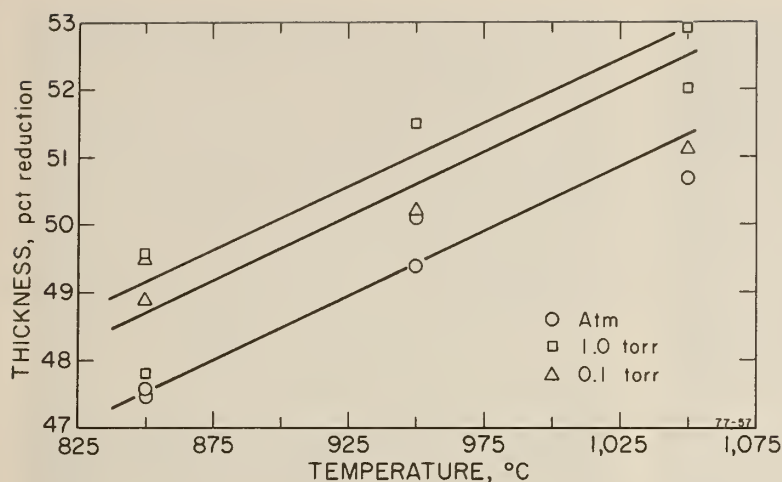


FIGURE 6. - Effect of atmosphere on reduction of Ti-6Al-4V.

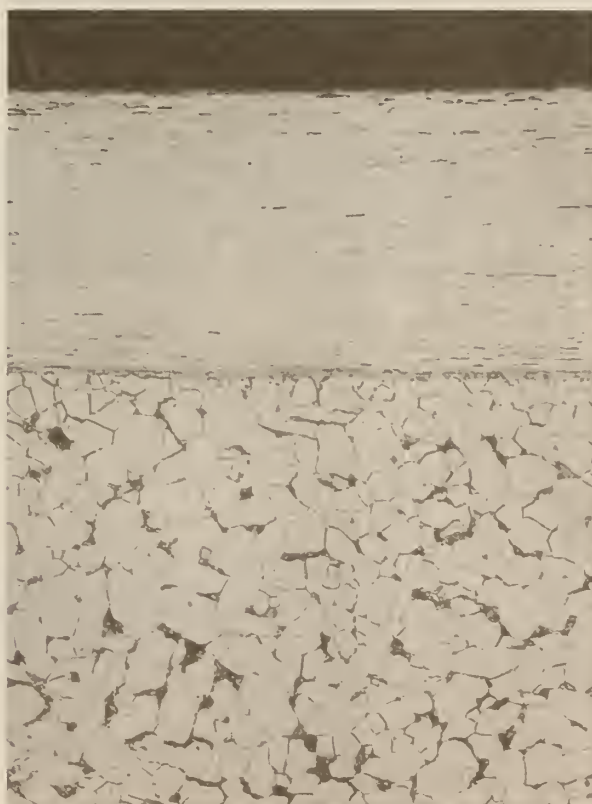
### Cladding by Rolling at Moderate Vacuum

Molybdenum was roll-bonded to both high-purity (99.9 percent) iron and steel. Although the specimens were all heated to 1,000° C, it is estimated that there was as much as 100° to 200° C temperature decrease in transfer from the furnace to the rolls. Figures 7-8 show the bond zone between low-carbon steel and molybdenum and between electrolytic (very low-carbon) iron and molybdenum after one and two

passes and after two and three passes, respectively. The bond zone became wider with the number of passes made, and wider between electrolytic iron and molybdenum than between steel and molybdenum. Upon examination by electron microprobe, one specimen showed diffusion of molybdenum into iron at a distance



A After one pass X 400



B After two passes X 400

FIGURE 7. - Interface between roll-bonded molybdenum and low-carbon steel.



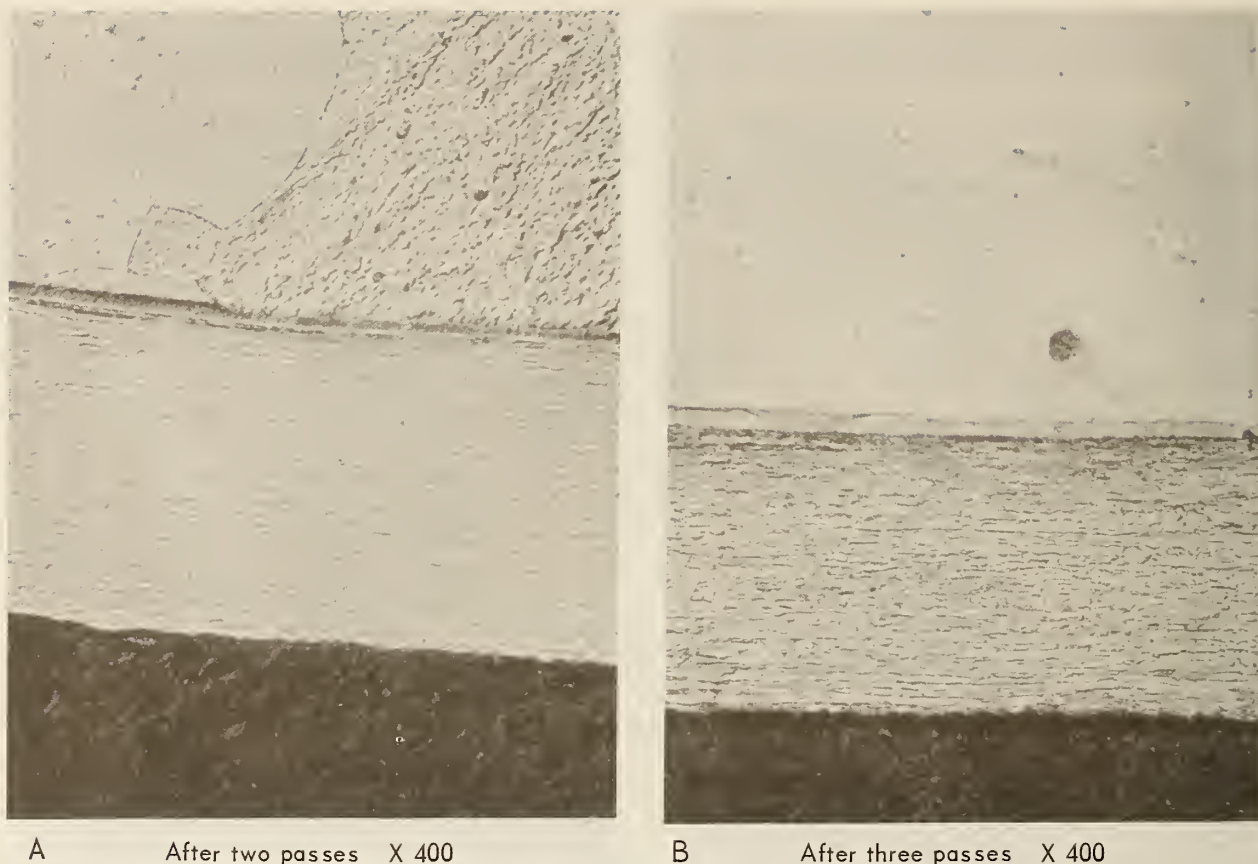


FIGURE 8. - Interface between roll-bonded molybdenum and electrolytic iron.

of 10 to 12 micrometers with about 4.2 wt-pct molybdenum at the center of the diffusion zone. Molybdenum diffused more readily into the pure iron than into the steel. A comparison is made in tables 1-2.

TABLE 1. - Roll-bond diffusion between molybdenum and electrolytic iron at 1 micrometer depth

| Reduction, pct | Mo into Fe,<br>wt-pct Mo | Fe into Mo,<br>wt-pct Fe |
|----------------|--------------------------|--------------------------|
| 10.....        | 0.3                      | Nil.                     |
| 20.....        | 10.5                     | Nil.                     |
| 30.....        | 9.5                      | Nil.                     |

TABLE 2. - Roll-bond diffusion between molybdenum and steel at 1 micrometer depth

| Reduction, pct | Mo into Fe,<br>wt-pct Mo | Fe into Mo,<br>wt-pct Fe |
|----------------|--------------------------|--------------------------|
| 10.....        | 0.4                      | 0.4                      |
| 20.....        | .4                       | .4                       |
| 30.....        | 5.0                      | .5                       |

An attempt was made to roll-bond thin molybdenum sheet to thin iron sheet. This was possible when the following procedure was followed: The sheets were cleaned by wire brush and pickled for 1/2 hour in hydrochloric acid, subsequently rinsed, dried rapidly, and spot-welded together by a small (500-watt) electric spot-welding machine (minimizing surface oxidation). The two sheets, 5-mil molybdenum and 10-mil iron, were further spot-welded at one end to a stainless steel bar (fig. 9). The bar served as a thermal stabilizer to keep the thin sections hot during transfer from the furnace to the rolls. Good bonding of thin sheet was accomplished by heating the pack to  $1,000^{\circ}\text{C}$  and rolling in a chamber pressure of  $6 \times 10^{-2}$  to  $1 \times 10^{-1}$  torr.

Bonding molybdenum to stainless steel and iron was accomplished after grinding the surfaces, cleaning with hydrochloric acid, and spot-welding first the electrolytic iron sheet to molybdenum sheet and then tacking them between sheets of 304 and 316 stainless steel. A cross section of the bonded four metals is shown in figure 10.

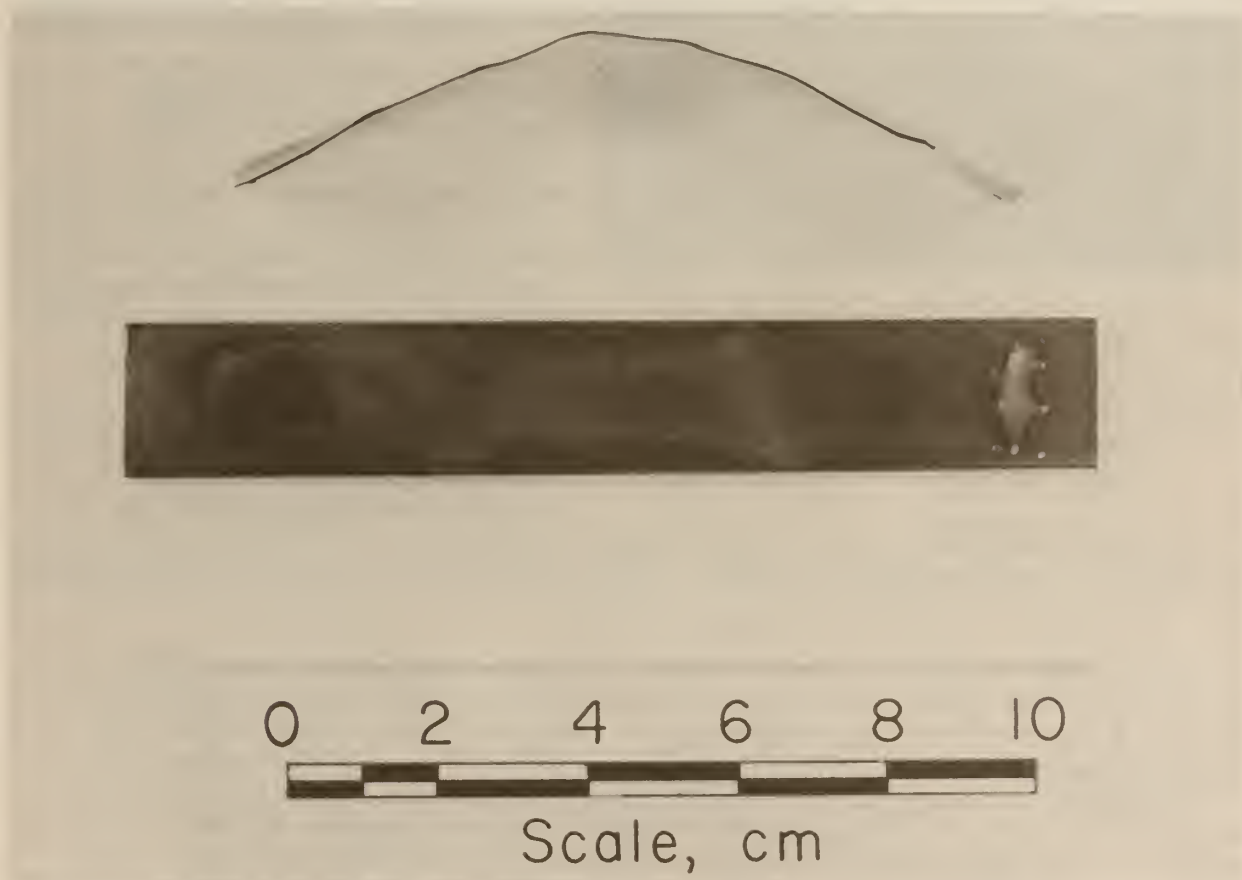


FIGURE 9. - Thin sheets of molybdenum roll-bonded to iron. (Molybdenum was 0.005 inch thick, iron was 0.010 inch thick; rolled upon a stainless steel bar, approximately  $900^{\circ}\text{C}$ , 20 pct reduction.)



One pass, 20 pct reduction, 1,000° C  
0.1 torr X 100

FIGURE 10. - Roll-bonded sandwich of top 304 stainless steel, electrolytic iron, molybdenum, and bottom 316 stainless steel.

1-1/2 inches in diameter while the backup rolls are 6-1/2 inches in diameter, all made of vanadium-type tool steel. Roll bearings are lubricated with silicone grease.

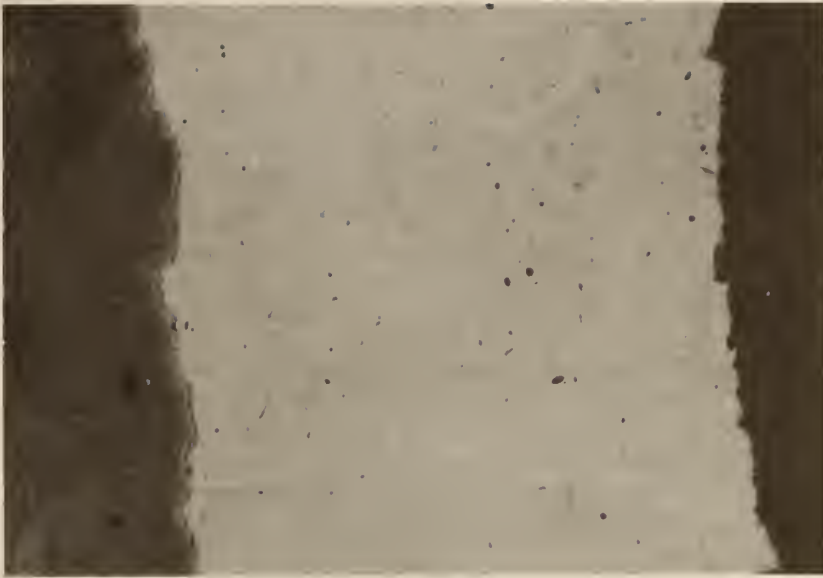
The vacuum chamber is constructed of 1-inch-thick steel plate and includes several 1-inch-thick glass windows to provide adequate visibility of all operations inside. A manipulator in the extension at each end of the chamber allows highly controlled specimen handling. A loading chamber on the entrance side of the mill has a third manipulator which is used to transfer specimens between the room and the rolling mill main chamber without breaking vacuum. The main chamber is pumped by two 6-inch-diameter diffusion pumps backed by a mechanical pump. Typical pressure in the chamber during hot rolling is 2 to 4  $\times 10^{-5}$  torr. The loading chamber is pumped by a separate 4-inch diffusion pump, cold trap, and mechanical pump.

Commercial-purity electrolytic chromium was hot-rolled from melted buttons to thin sheet at about  $10^{-1}$  torr pressure with little difficulty. Roll-bonding chromium to high-purity iron was accomplished, but only after cleaning all surfaces in hydrochloric acid and spot-welding the chromium sheet to the iron. The bond was accomplished by heating to 1,000° C and using a very high reduction (over 60 percent) at  $1 \times 10^{-1}$  torr pressure. One such bond is shown in figure 11.

#### Description of New Equipment

A second vacuum rolling mill facility was put into operation recently. The unit consists of a 50-ft<sup>3</sup> vacuum chamber which encloses a rolling mill and furnace, as illustrated in figure 12. A 40-hp mill motor and drive gears are outside the chamber. The rolling mill and vacuum chamber were previously located at the University of California, Lawrence Livermore Laboratory (26). The mill has a separating force capacity of 175,000 pounds. The rolls have an 8-inch face and, as a four-high mill, the work rolls are





One pass, 60 pct reduction, 1,000° C 0.1 torr X 600

FIGURE 11. - Electrolytic iron-chromium bond.

The specimen heating furnace, with its low-mass and minimum-surface area, can be heated rapidly with very little outgassing. It is provided with a tantalum split-resistor element of 3-inch-diameter and 10-inch-length inside a quartz tube, and is capable of heating to at least 1,200° C. The quartz tube electrically insulates the heating element from the four radiation shields. At a temperature of 1,000° C, the power in the furnace circuit is approximately 250 amp at 6 v. Doors on the ends of the furnace minimize

radiation end losses and are controlled from outside the chamber.

During rolling, the specimen is transferred to the furnace and rolls while on a specimen carrier, figure 12. By moving the carrier forward, the specimen is brought to the middle of the furnace where it reaches temperature

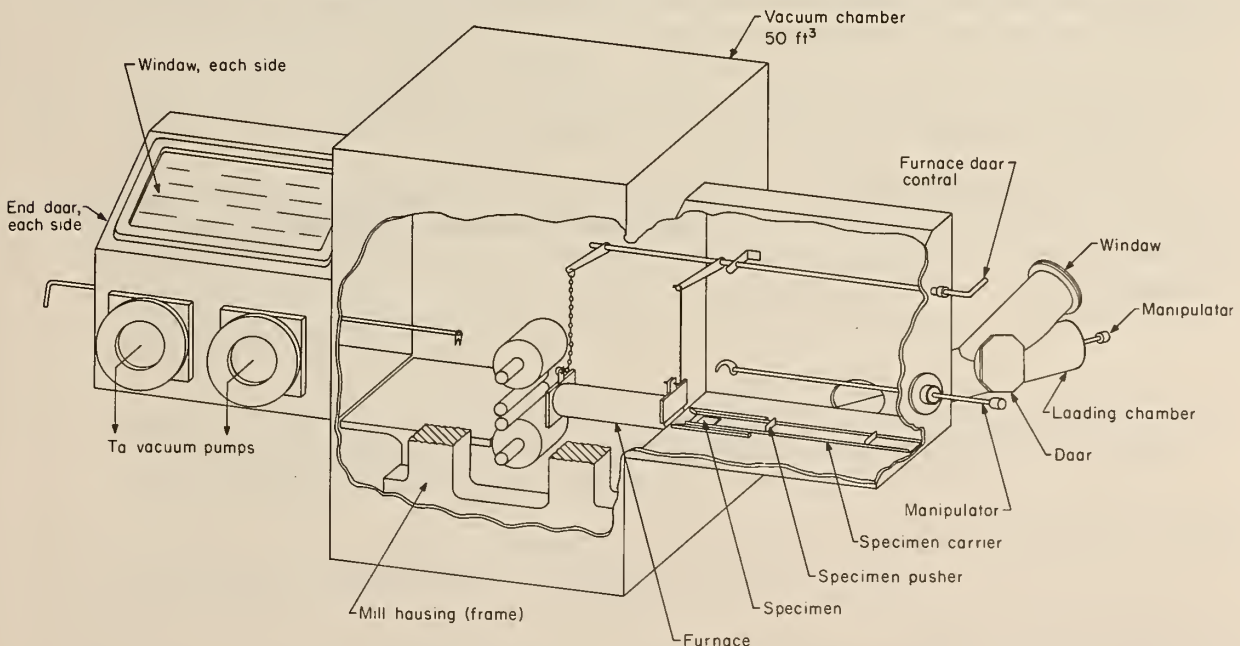


FIGURE 12. - New facility, vacuum rolling mill.

in about 8 minutes. Further advance of the carrier transfers the specimen to the rolls. If the specimen does not immediately feed into the rolls, it can be fed by advancing the specimen pusher. Because only a few seconds are required to transfer the specimen from the furnace to the mill, the temperature of the specimen drops very little. Furthermore, the hot specimen carrier helps maintain the specimen temperature. During calibration runs, in which a thermocouple was attached to a specimen, the temperature drop was found to be less than  $15^{\circ}\text{C}$  at  $1,000^{\circ}\text{C}$ .

#### DISCUSSION AND CONCLUSIONS

From the literature review, it is apparent that considerable attention has been paid to vacuum rolling in the U.S.S.R. It is not certain that the activity has moved beyond the laboratory to the production stage except for tube production. In the United States, despite researchers attempts to gain Government or industrial support for development in the area, most requests have not found support. Vacuum rolling obviously can be practical only when costs by conventional methods are excessive, or when present techniques do not produce the necessary product.

Titanium is a good example of what can be accomplished with vacuum rolling; it also can be rolled in air. The practice of one major titanium producer is to sheath it in iron, roll, and then strip to obtain the quality required. The extra costs of this operation could lead to consideration of vacuum rolling, even though no property improvement is gained.

Molybdenum also can be rolled in air. But nowhere in the literature has preparation of stainless steel-clad molybdenum been reported. The possibilities of obtaining hot strength with oxidation resistance by this composite should be tempting to design engineers.

Chromium of commercial purity can be rolled in vacuum to form sheet. It further can be bonded to steel in a low-pressure operation.

The commercial utility of vacuum hot rolling of metals only can be conjectured at this time. It will be necessary to obtain further property data to establish whether there are genuine reasons to pursue this difficult but clean process.



REFERENCES<sup>5</sup>

1. Aleksandrov, A. A., A. S. Tron', and N. Rybal'chenko. (Production of Nickel-Copper Bimetal by Vacuum Rolling.) Polytechnicheskii Institut. Trudy (Leningrad), Mashiny i Tekhnologiya Obrabotki Metallov Davleniyem, No. 263, 1966, pp. 42-47 (in Russian); Eng. Transl. FTD-MT-24-264-67, Air Force Systems Command, pp. 5-11.
2. Amonenko, V. M., V. M. Godin, E. A. Kovaleva, A. S. Tron', and A. F. Yakushin. (Production of Strong Titanium-Steel Bimetals by Vacuum Rolling.) Tsvetn. Metal., v. 40, No. 12 (in Russian); v. 8, No. 12, 1967, pp. 55-58 (Eng. Transl.).
3. Amonenko, V. M., A. S. Tron', and V. V. Mukhin. (Properties of Bimetal Ni-Cu and Ni-Cu-Ni Obtained by Vacuum Rolling.) Tsvetn. Metal., v. 41, No. 9 (in Russian); v. 9, No. 9, 1968, pp. 121-124 (Eng. Transl.).
4. Amonenko, V. M., A. S. Tron', V. V. Mukhin, N. D. Rybal'chenko, and E. A. Kovaleva. (Producing Bimetals by Vacuum Rolling and Their Properties.) Tsvetn. Metal., v. 39, No. 12 (in Russian); v. 7, No. 12, 1966, pp. 90-92 (Eng. Transl.).
5. Amonenko, V. M., A. S. Tron', V. V. Mukhin, and V. A. Tarasov. (A Vacuum Rolling Mill.) Stal', v. 10, October 1960, pp. 749-751; English translation by British Iron and Steel Industry Translation Service, The Iron and Steel Institute, London, BISI 3744, June 1964, 5 pp.
6. Anikeev, N. A., Ya. B. Gurevich, I. M. Pavlov, A. V. Krupin, and V. L. Orzhekhovsky. Mass-Spektrometricheskii Analiz Gazov Pri Prokatke V Vakuume (Mass Spectrometric Analysis of Gases in Vacuum Rolling). Izv. Vysshikh Uchebn. Zavedenii, Chernaya Met., v. 7, 1969, pp. 96-100.
7. Bianchi, L. M., and C. P. Mueller. The Mechanical Working of Metals in Vacuum or Inert Atmospheres. Proc. 4th Internat. Conf. on Vacuum Metallurgy; the Iron and Steel Institute of Japan, Kenkyusha Printing Co., Ltd., Tokyo, 1974, pp. 325-328.
8. Blickensderfer, R. Laboratory Apparatus for High Temperature Forging Under Vacuum or Inert Atmospheres. Rev. Sci. Instr., v. 43, No. 6, June 1972, pp. 947-948.
9. Bonchak, J., and L. M. Bianchi (assigned to Universal Cyclops Specialty Steel Division). Method of Cladding Metals and Composites Thereof. U.S. Pat. 3,606,103, Sept. 14, 1971.
10. Bykadorov, A. T. (The Strength and Ductility Properties of Steels Rolled in Vacuo.) Stal', No. 1, January 1968, pp. 43-44.

---

<sup>5</sup>Titles enclosed in parentheses are translations from the language in which the item was published.

11. Bykadorov, A. T., D. I. Shetulov, L. D. Sokolov, and A. N. Gladkikh. Prochnost' i Plastichn Ost' Nekotorkh Staley Prokatann'kh Vakuume (Strength and Plasticity of Some Steels Rolled in Vacuum). Izv. Vysshikh Uchebn. Zavedenii Chernaya Met., v. 11, No. 10, 1968, pp. 102-104 (in Russian); partial English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.
12. Carter, F. R. Effects of Temperature and Pressure on Contamination of Refractory Metals. World Metal Show, Conf. 53-6, New York, Oct. 29-Nov. 2, 1962, 42 pp.
13. Chernyshev, V. N., A. V. Krupin, V. G. Osipov, Yu. L. Farapin, V. L. Linesky, and V. G. Golovekenko. Nalipanie Metalla Na Valki Pri Prokatke v Vakuume (Adherence of Metal on the Rollers During Rolling in Vacuo). Plastic. Deform. Tugopl. Metallov i Special., Izd. Nauka (Moscow), ed. by I. M. Pavlov, 1970, pp. 55-60 (in Russian); English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.
14. Chernyshev, V. N., A. V. Krupin, and Yu. P. Vorobev. (Comparison of the Kinematic Process Conditions During Rolling in Vacuum and in Air.) Izv. VUZ Chernaya Met., v. 4, No. 11, 1974, pp. 86-88 (in Russian); Steel (USSR), v. 4, No. 11, November 1974, pp. 906-909 (Eng. Transl.).
15. Dolzhenkov, F. E., and Yu. I. Krivonosov. (Cohesion Strength Titanium-Steel Bimetal Layers Under Vacuum Rolling.) Tsvetn. Metal., v. 37, No. 6 (in Russian); v. 5, No. 6, 1964, pp. 65-67 (Eng. Transl.).
16. Dolzhenkov, F. E., Yu. I. Krivonosov, and L. A. Zakharov. (Rolling the Titanium-Steel Bimetal in a Vacuum and a Neutral Atmosphere.) Tsvetn. Metal., v. 39, No. 6, 1966 (in Russian); v. 7, No. 6, June 1966, pp. 85-88 (Eng. Transl.); U.S. Department of Commerce, TT-66-33953, JPRS: 37.525, Sept. 9, 1966, pp. 23-28.
17. Dolzhenkov, F. E., Yu. I. Krivonosov, D. I. Piryazev, and L. A. Zakhovov. (Producing Bimetals by Rolling in Vacuum.) Tsvetn. Metal. (Moscow), No. 6, June 1966, pp. 77-80 (in Russian); Stal', No. 1, January 1969, pp. 67-68 (Eng. Transl.).
18. Gurevich, Ya. B., A. P. Baschenko, and V. L. Orzhekhovskiy. (Hot Rolling of High-Melting-Point Metals Under Vacuum and in an Inert Gas.) Tsvetn. Metal., v. 38, No. 7, 1965, pp. 76-81 (in Russian); Soviet J. Non-Ferrous Metals, v. 6, No. 7, pp. 87-92 (Eng. Transl.); English translation by H. Bratcher, Technical Translations, No. 6444, Alladena, Calif., 1965, 12 pp.
19. Gurevich, Ya. B., and V. L. Orzhekhovskiy. (Plastic Deformation of Refractory Metals in a Vacuum.) Probl. Metalloved. i Fiz. Metal., No. 58, 1968, pp. 198-211 (in Russian); English translation by Foreign Technology Division, Wright Patterson Air Force Base, Ohio, FTO-HT-23-583-72, Sept. 8, 1972, 18 pp.

20. Gurevich, Ya. B., Yu. L. Zarapin, S. V. Zemskii, and A. V. Krupin. (Interaction of Metal With the Rolls During Hot Rolling in Vacuum.) Metalloved. i Term. Obrabotka Metal., No. 11, November 1969, pp. 52-54 (in Russian); English translation by Central Scientific Research Institute of Ferrous Metallurgy MISiS, Consultants Bureau, Plenum Publishing Corp., New York.
21. Gurevich, Ya. B., and A. M. Zubko. Friction Coefficient and Specific Pressure When Hot Rolling in a Vacuum. Stal', Oct. 10, 1959, pp. 929-932.
22. Habermann, C. E., A. L. Rafalski, and R. D. Hansen. A High Temperature Forge for Refractory Metals. J. Less-Common Metals, v. 18, No. 2, June 1969, pp. 105-109.
23. Hill, M., R. Holman, and E. Kulkinski. Equipment for Hot Rolling Strip in Vacuum. Trans. 6th Nat. Symp. on Vacuum Technology, Philadelphia, Pa., Oct. 7-9, 1959; pub. by Pergamon Press, New York, ed. by C. R. Meissner, 1960, pp. 124-128.
24. Industrial Heating. Aspects of Vacuum and Inert Gas Fabricating Atmospheres for Refractory Metals. V. 29, No. 6, June 1962, pp. 1084-1094.
25. Iron Age. New Plant for Refractory Metals Will Feature Inert Atmosphere. V. 182, No. 20, November 1958, pp. 148-149.
26. \_\_\_\_\_. Vacuum-Purged Mill Rolls Strip. V. 189, No. 7, February 1962, p. 115.
27. Ivanov, E., S. F. Kovtyn, N. D. Tarasov, and R. A. Ul'yanov. (Vacuum Rolling for Chemically Active Metals.) Tsvetn. Metal., v. 35, No. 11, 1962, pp. 85-88 (in Russian); Soviet J. Non-Ferrous Metals, v. 2, No. 11, 1962, pp. 84-86 (Eng. Transl.).
28. Kelman, L. R., W. D. Wilkinson, A. B. Shuck, and R. C. Goertz. Handling Alpha-Active, Pyrophoric Materials. Nucleonics: Part 1. What is the Best Approach, v. 14, No. 3, March 1956, pp. 61-65; Part 2. Glovebox Design and Construction, v. 14, No. 4, April 1956, pp. 65-71; Part 3. Glovebox Atmosphere Control, v. 14, No. 5, May 1965, pp. 77-82.
29. King, T. B. Thermodynamics and Kinetics in Vacuum Metallurgy and the Effect of the Pressure Variable. Lecture No. 3, Vacuum Metallurgy Course (Lecture Series 23), New York University, June 10-14, 1957, pp. 337-358.
30. Kolbe, C. L. Inert Gas Forging. J. Electrochem. Soc., v. 101, No. 12, December 1954, pp. 601-603.



31. Kolikov, A. P. (Workability of Refractory Metals in Helical Rolling in Different Atmospheres.) *Izv. VUZ Chernaya Met.*, v. 7, 1976, pp. 80-83 (in Russian); English translation by British Industrial and Scientific International Translation Service, The Metals Society, London, BISI 14904, Mar. 9, 1977, 4 pp.
32. Krivonosov, Yu. I., F. D. Dolzhenkov, O. A. Myakshin, and L. A. Zakharov. (Producing the Bimetal Niobium-Steel by Vacuum Rolling.) *Tsvetn. Metal.*, v. 39, No. 12 (in Russian); v. 7, No. 12, 1966, pp. 103-104 (Eng. Transl.).
33. Krupin, A. V. Das Walzen im Vakuum (Rolling in Vacuum). *Proc. 7th Plansee Seminar on Powder Metallurgy of High Temperature Metals, Institute of Steel and Alloy (Moscow), Rentte-Tyrol (Austria); Metallwerk Plansee, ed. by F. Benesvosky, v. 4, 1971, pp. 19.1-19.24; English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Ore.*
34. Krupin, A. V., and V. N. Chernyshev. Rolling of Metals in Vacuum. *Proc. 4th Internat. Conf. on Vacuum Metallurgy; pub. by the Iron and Steel Institute of Japan, Kenkyusha Printing Co., Ltd., Tokyo, 1974, pp. 329-332.*
35. Krupin, A. V., and I. M. Pavlov. Treatment of Metals and Bimetals in Vacuum. *Metallurgia*, No. 46, 1968, p. 27.
36. \_\_\_\_\_. (Research on Rolling Metals Under Vacuum.) *Izv. Akad. Nauk SSSR-Metal.*, No. 3, May-June 1968, pp. 118-120 (in Russian); *Metallurgist (USSR) (English Transl. of Metallurgy)*, No. 3, May-June 1968, pp. 84-85.
37. Krupin, A. V., I. M. Pavlov, V. N. Chernyshev, V. S. Bogolyubov, and B. L. Linetskii. (A 210 mm Mill for Rolling Under Vacuum.) *Vestn. VUZ Chernaya Met.*, v. 12, No. 3, March 1965, pp. 89-93 (in Russian); English translation by H. Bratcher, Technical Translations, No. 6516, Alladena, Calif., 1965, 8 pp.
38. Krupin, A. V., I. M. Pavlov, B. L. Linetskii, V. N. Chernyshev, Yu. L. Zarapin, V. N. Starkov, P. A. Korchagin, V. V. Vinogradov, and T. V. Tyukalov. (Rolling Tungsten and Molybdenum in an Atmosphere With Low Partial Oxygen Pressure.) *Tsvetn. Metal.*, May 1966, pp. 108-109.
39. Krupin, A. V., and N. V. Yudina. (Rolling of Metals and Bimetals in Vacuum.) *Institut Nauchnoy Informatsii. Prokatnoye i Volochetnoye Proizvodstvo, 1965. Itogi Nauki i Tekhniki, Seriya: Metallurgiya (Moscow), 1966, pp. 131-168 (in Russian); English translation by Foreign Technology Division, Wright Patterson Air Force Base, Ohio; available from National Technical Information Service (formerly Clearinghouse for Federal Scientific and Technical Information), Springfield, Va., FTD-MT-24-197-67, Sept. 8, 1967, 32 pp.*



40. Nel'zin, L. N., and P. F. Filippov. (Effect of Vacuum Rolling on the Plastic Properties of Titanium Alloys.) *Tsvetn. Metal.*, v. 42, No. 2 (in Russian); v. 10, No. 2, February 1969, pp. 85-86 (Eng. Transl.).
41. Osipov, V. G., A. V. Krupin, Fu. L. Farzpin, V. N. Tchernyshev, Ya. B. Gurevich, and V. L. Orzhekhovskiy. *Issledovanie Protesessa Prokatki Vol'frama V. Vakuume* (Investigation of the Process of Rolling Tungsten in Vacuum). *Plastic Deformation of Refractory Metals*, ed. by I. M. Pavlov. *Izdatel'stvo Nauki* (Moscow), 1970, pp. 34-36; NSA, v. 26, No. 1, p. 456 (in Russian); English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.
42. Pavlov, I. M., V. L. Orzhekhovskiy, Ya. B. Gurevich, and A. Ye. Shelest. (The Effect of the Roll Material and Surface Finish on Some Parameters of Hot Rolling in Vacuum.) *Russian Met. and Min.*, No. 1, January-February 1963, pp. 4-9.
43. Pevzner, S. B., N. I. Korneyev, I. G. Skugarev, A. S. Tugushev, Yu. V. Malashenko, and V. B. Yeml'yanov. (Forging of Refractory Metals in Vacuum.) *Tsvetn. Metal.* (Moscow), v. 8, No. 8, August 1967, pp. 86-88 (in Russian); English translation available from U.S. Department of Commerce, Springfield, Va., TT 67-33640, JPRS: 43.015, Oct. 18, 1967, 5 pp.
44. Polukhin, P. I., A. V. Krupin, A. P. Kolikov, I. N. Potapov, E. N. Larin, S. A. Kozeradskii, and V. I. Gladkov. (Investigation of Processes of Vacuum Rolling Tube Billets. Communication I.) *Steel (USSR)*, v. 4, No. 4, April 1974, pp. 61-65.
45. \_\_\_\_\_. (Investigation of Processes of Rolling Tube Billets in Vacuum. Communication 2.) *Izv. VUZ Chernaya Met.*, No. 9, 1974, pp. 80-84 (in Russian); English translation by British Industrial and Scientific International Translation Service, The Metals Society, London, BISI 12890, January 1975, 4 pp.
46. Rossin, P. C., and C. P. Mueller. Current and Potential Uses of Vacuum and Inert Atmosphere Fabrication Processes. *Proc. Electric Furnace Conf.*, AIME, Pittsburgh, Pa., Dec. 6-8, 1961, v. 19, pp. 8-22.
47. Sadaj, J. *Bimetale* (Bimetals). *Fudy i Metale Niezelazne*, v. 18, No. 1, 1973 (in Polish); English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.
48. Semchyshen, M., and R. Q. Barr. Arc Cast Molybdenum-Base Alloys, Summary Report. Climax Molybdenum Co. of Michigan, to Office of Naval Research, No. NR 039-002, 1955, p. 145.
49. Sigalov, J. M., and K. Exerskii. *Polupromyshlennyy Vakuumnyy Prokatnyy Stan Duo-400* (Treatment of Metals and Bimetals in Vacuum). *Metallurgia*, No. 46, 1968, pp. 49-53.

50. Smirnov, V. S., A. A. Aleksandrov, and L. A. Shibarov. Ustandvka Dlya Prokatki Metallov V Vakuume Ili Srede Gazov Inertn'h (Assembly for the Rolling of Metals in Vacuum and in an Atmosphere of Inert Gases). Trudy LPI No. 238, 1964, pp. 81-89; English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.
51. Smirnov, V. S., V. M. Amonenko, A. S. Tron', and A. A. Aleksandrov. Vliyanie Prokatki V Vakuume Na Svoystva Metallov (Effect of Vacuum Rolling on Metal Properties. In Metal Working by Pressure). Trudy LPI No. 238, 1964, pp. 95-100; English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.
52. Smirnov, V. S., O. F. Danilevskii, A. A. Aleksandrov, V. I. Stol'nyi, and E. S. Kagan. (Manufacture of Bimetallic Sheets by Rolling Vacuum Packs.) Stal', No. 11, 1966, pp. 901-902.
53. Smirnov, V. S., A. S. Tron', A. A. Aleksandrov, Ya. M. Vitroskii, and N. D. Rybalchenko. Vliyanie Vakuumnoy Prokatki Na Strukturu I Gazonas'shenie Titana I Molibdena (Effect of Vacuum Rolling on the Structure and Gas Saturation of Titanium and Molybdenum). Polytechnicheskiy Institut. Trudy (Leningrad), No. 238, 1964, pp. 90-94 (in Russian); English translation available from Albany Metallurgy Research Center, Bureau of Mines, Albany, Oreg.
54. Smirnov, V. S., V. P. Yakovlev, and A. A. Aleksandrov. (Rolling of Beryllium in Vacuo.) Tsvetn. Metal., v. 46, No. 3, 1973, pp. 56-57.
55. Steel. The Plant That Outlaws Air. V. 139, No. 17, Oct. 22, 1956, pp. 78-79.
56. \_\_\_\_\_. Vacuum, Inert Atmospheres To Gain Favor in Forming. V. 150, No. 11, Mar. 12, 1962, pp. 80-81.
57. Tsygankov, E. M., and L. A. Perfil'ev. Research at Works Laboratories and Institutes. Stal', No. 11, 1964, p. 919.
58. Winter, J. (assigned to Olin Mathieson Chemical Corp.). Method of Forming a Composite Metal by Rolling and Recrystallization. U.S. Pat. 3,634,926, Jan. 18, 1972.













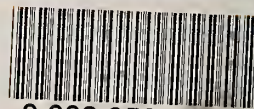
MAY 79



N. MANCHESTER,  
INDIANA 46962



LIBRARY OF CONGRESS



0 002 959 770 4